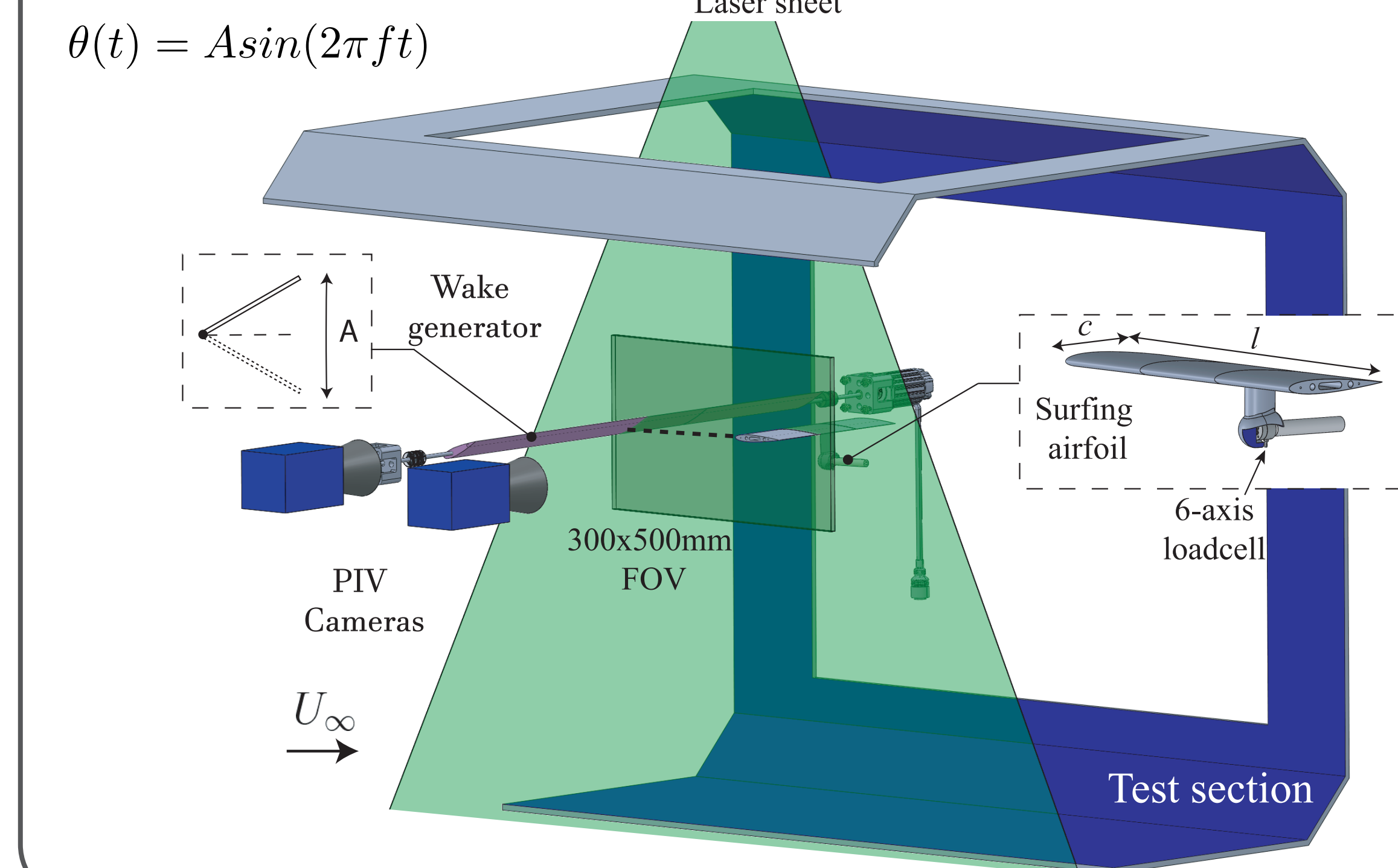


MOTIVATION

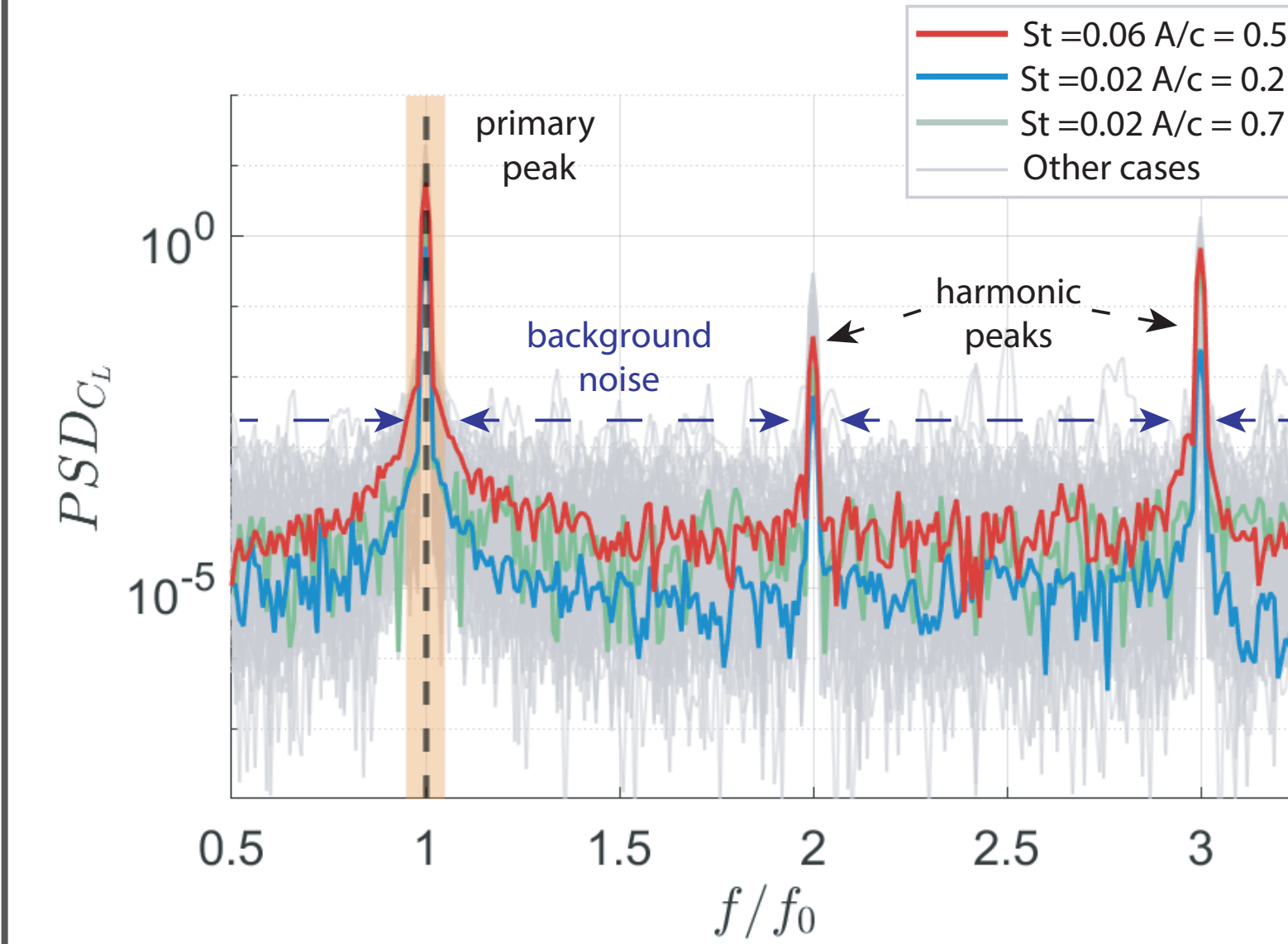
- Understand the aerodynamic force variation on a wing surfing in an unsteady 2-D wake
- Determine dependence of the overall lift fluctuations on the up-stream flapping kinematics
- Provide further interpretation of the dynamics in animal flocking

EXPERIMENTAL SETUP

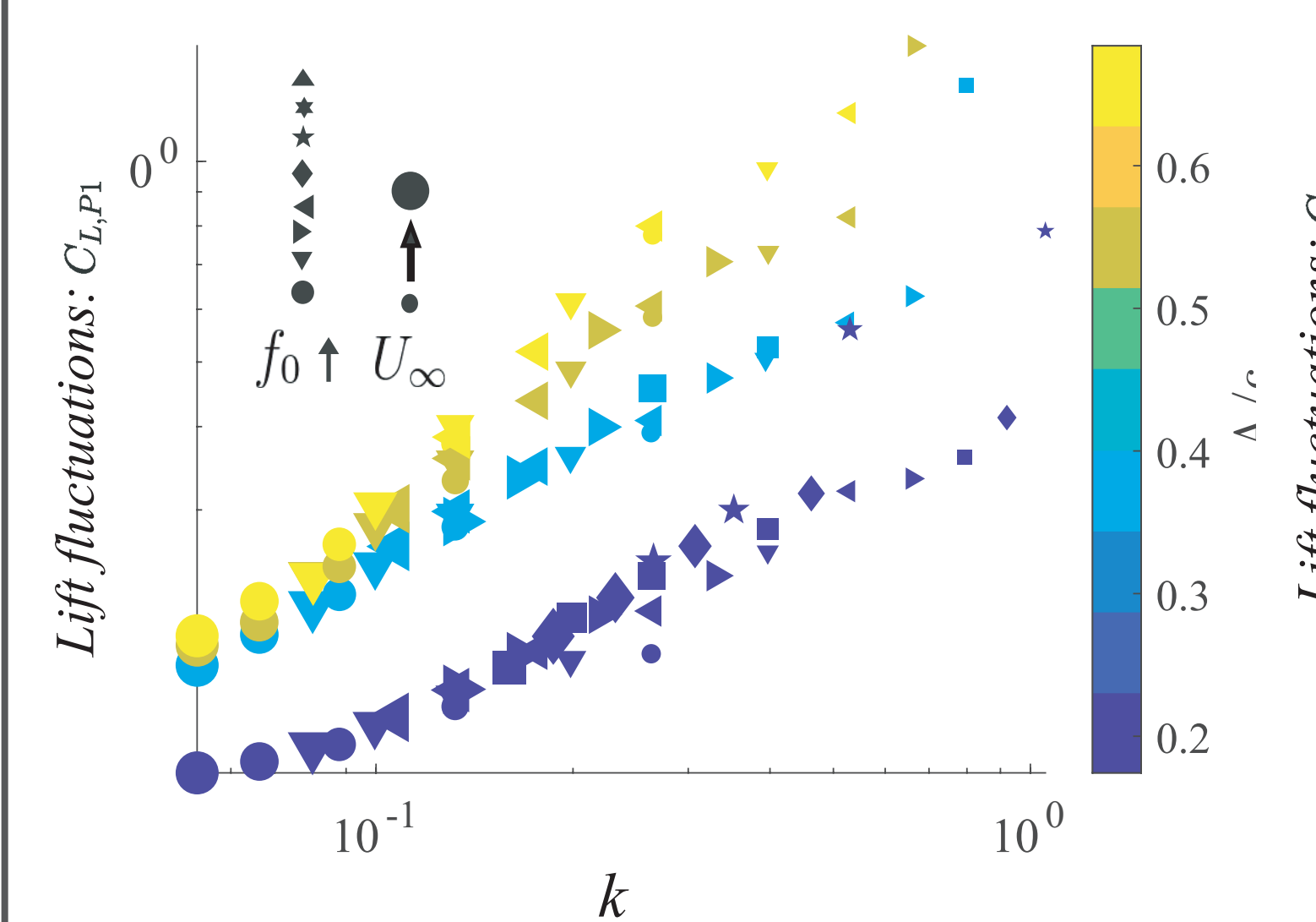
- A servo-driven wake generator with a flat plate pitching sinusoidally upstream.
- A NACA 0012 wing, placed 350 mm downstream, was mounted on a load cell to measure forces at 5000 Hz over 100 cycles.
- Vortex dynamics were captured via 2D2C PIV.
- The entire setup was automated by Matlab, with synchronized data acquisition.



CYCLE-LEVEL LIFT FLUCTUATIONS



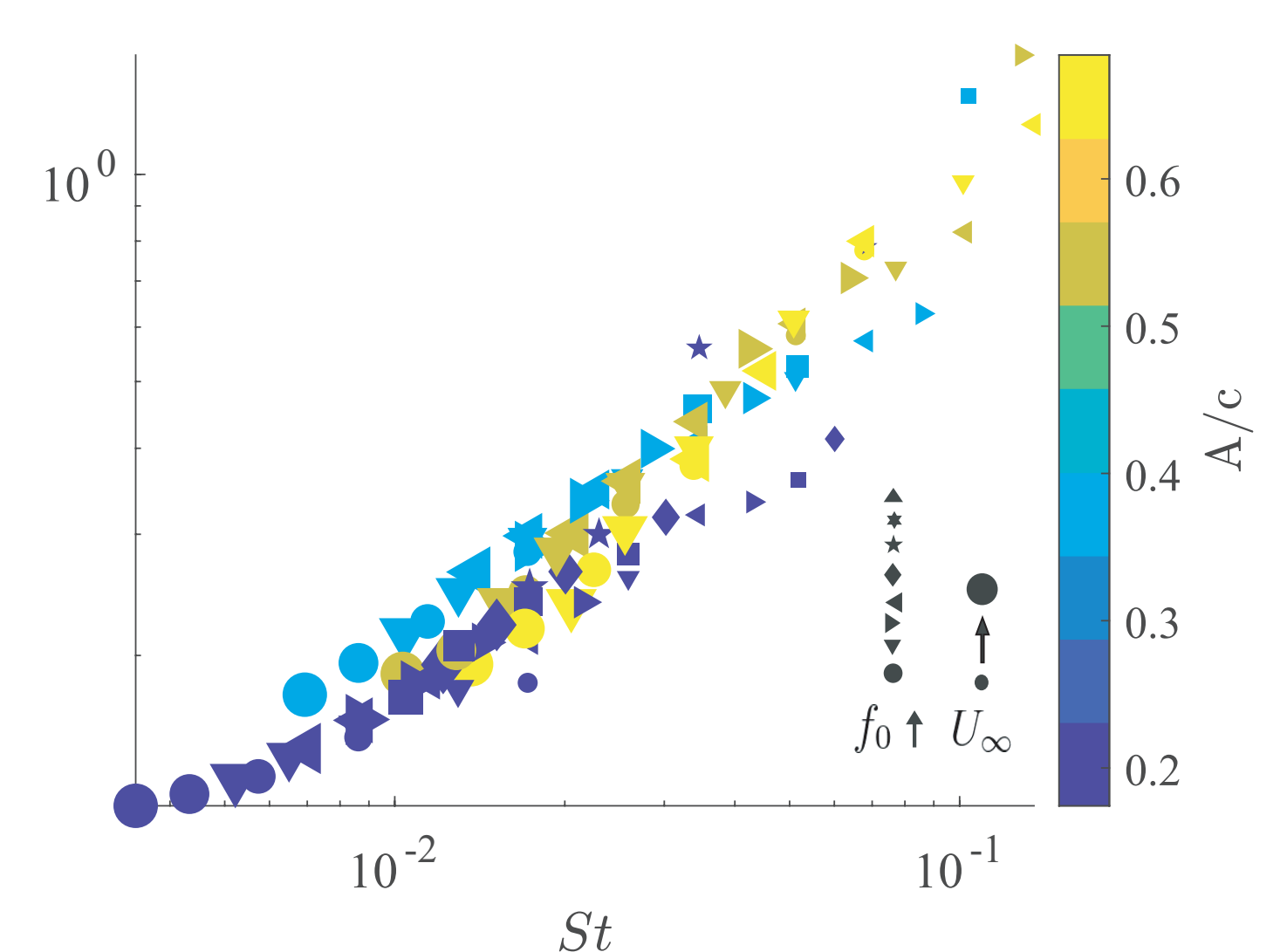
A. Power spectral density (PSD_{C_L}) of the lift coefficient for all measurements, with the example cases highlighted. The majority of the spectral energy (58%-99%) are distributed in the primary peak (highlighted in orange).



B. Narrow band integral

$$C_{L,P1} = \sqrt{\int_{0.95}^{1.05} PSD_{C_L} d\frac{f}{f_0}}$$

is used to quantify the cycle-level lift fluctuation.



C. To account for this A/c and k deviation, is plotted as a function of the Strouhal number, $St = fA/U_\infty$

PHASE-RESOLVED LIFT PREDICTION WITH UNSTEADY AERODYNAMICS

Time-domain approach $C_{L,W}(t) = \left[C_{L,QS,2D}(0) \Phi(\tau) + \int_0^\tau \Phi(\tau - \tau_0) \frac{dC_{L,QS,2D}}{d\tau_0} d\tau_0 \right] \frac{AR}{AR+2}$

Duhamel's integral

Wagner (or Küssner) function

Sears function

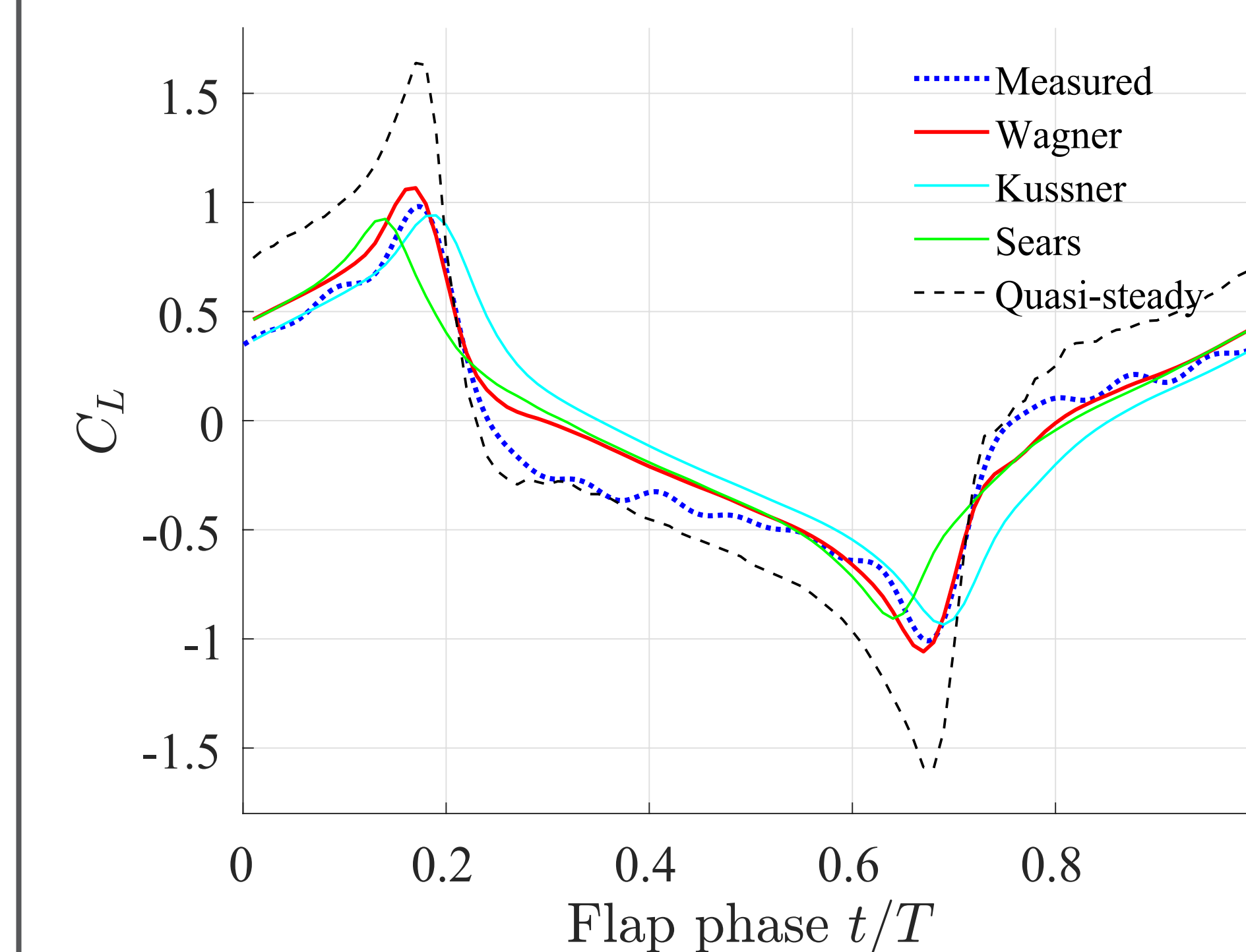
Frequency-domain approach $C_{L,S}(t) = \mathcal{F}^{-1} \{ \mathcal{F} \{ C_{L,QS,2D}(t) \} \cdot S(k) \} \frac{AR}{AR+2}$

Aspect Ratio Correction

$\tau = \frac{2tu}{c}$

$k = \frac{\pi cf}{U_\infty}$

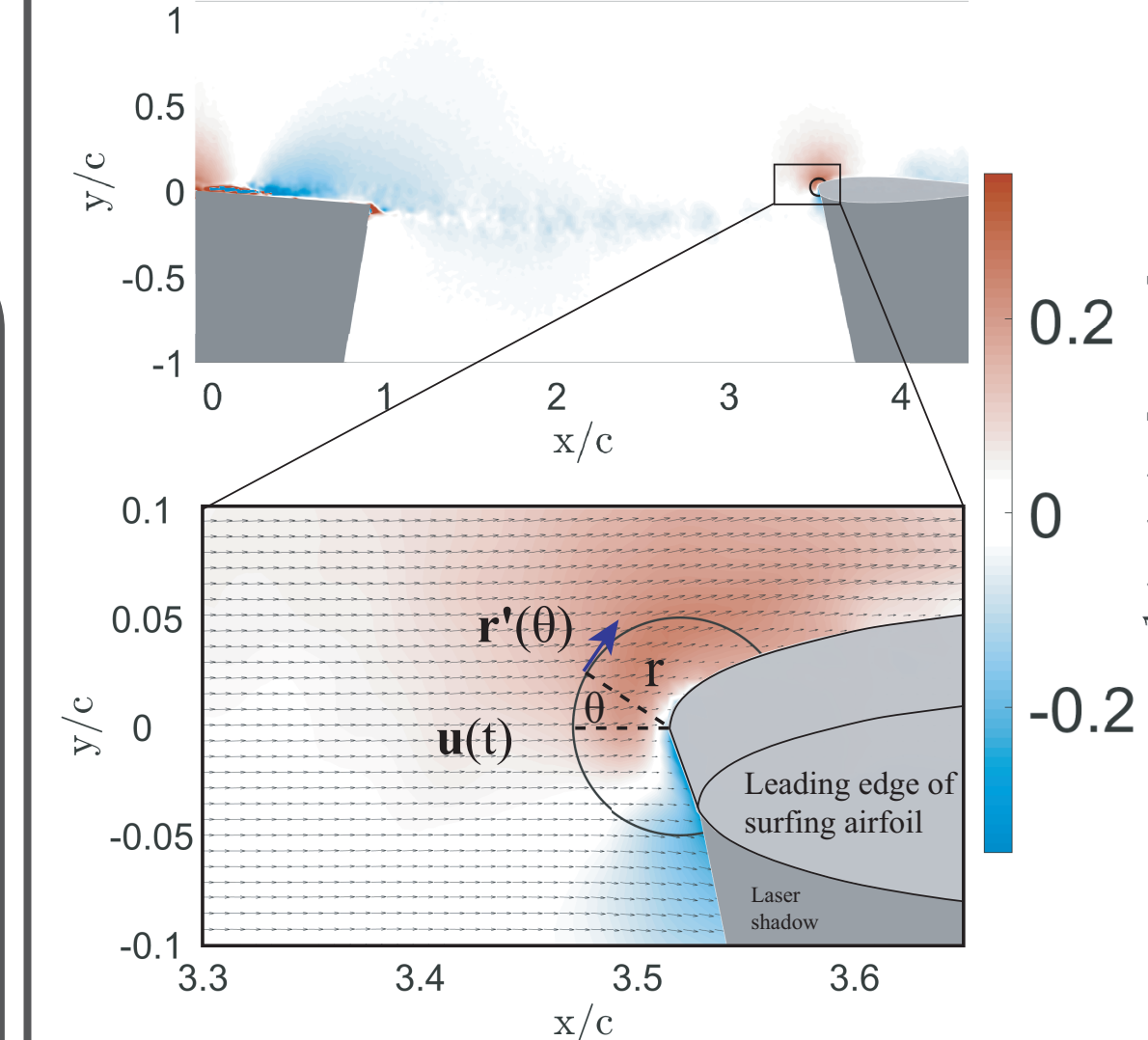
A.



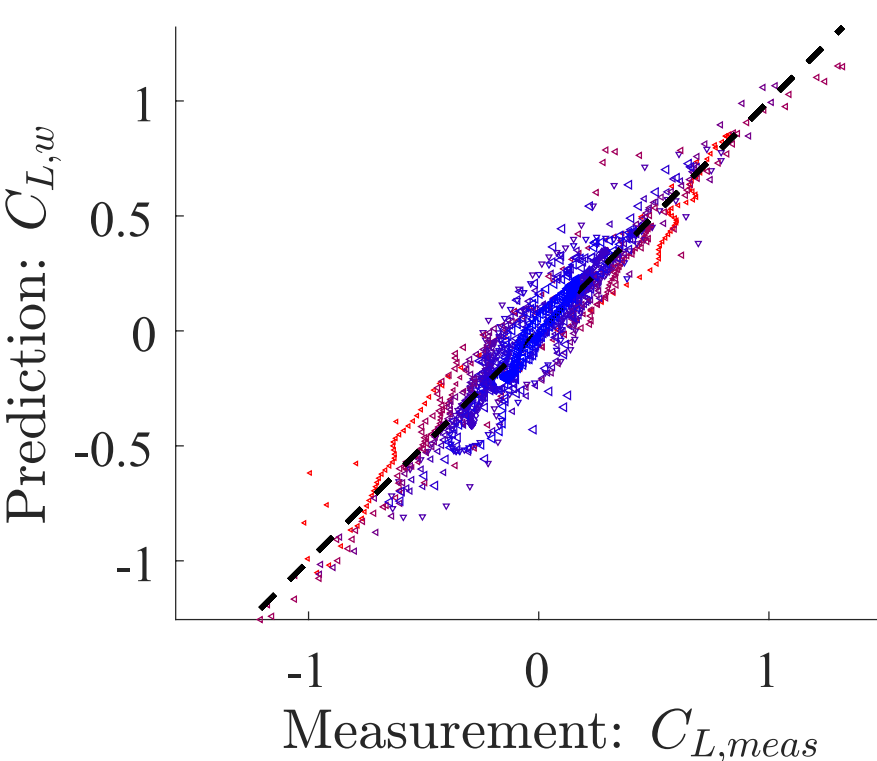
A. Comparison of unsteady approaches

- Quasi-steady approach shows a massive over prediction.
- The Wagner function with Duhamel's integral has the closest prediction compared to the directly measured data
- The Küssner function with Duhamel's integral exhibits a greater phase delay
- Sear's function applied with Fourier synthesis has good estimation of amplitude but lacks phase-wise accuracy in this case

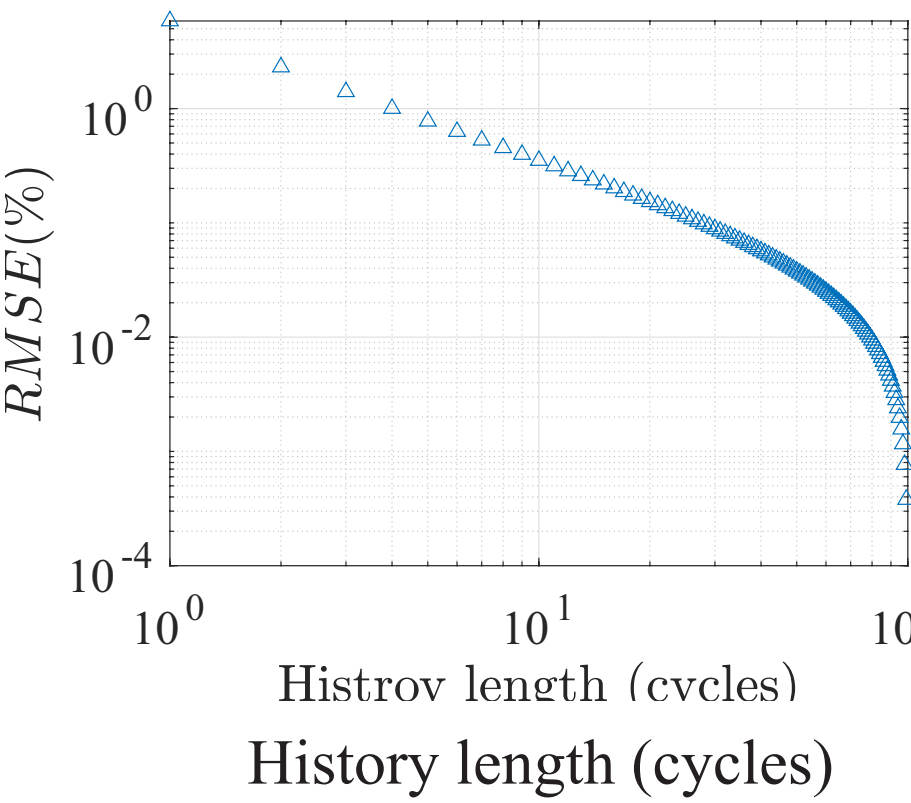
B.



C.



D.



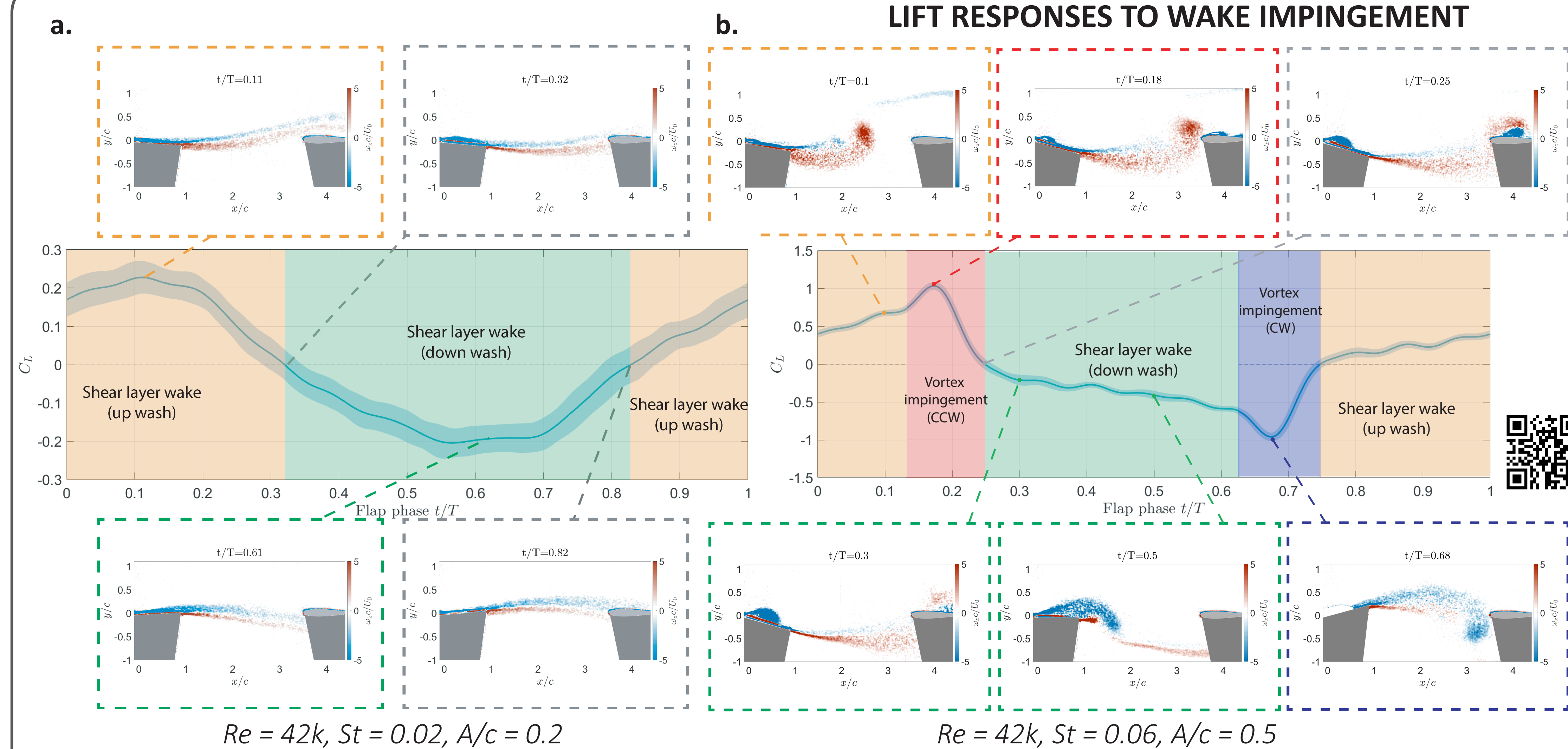
C. Frame-by-frame comparison of calculated vs. measured lift coefficient for various St numbers (14 cases, 1400 frames) by Wagner approach.

D. Convergence of the predictions: $RMSE = RMS(C_{L,w,cycn} - C_{L,w,cyc100}) / C_{L,max}$ of the Wagner approach as a function of time history length included in the calculation comparing with the final result with 100 cycles

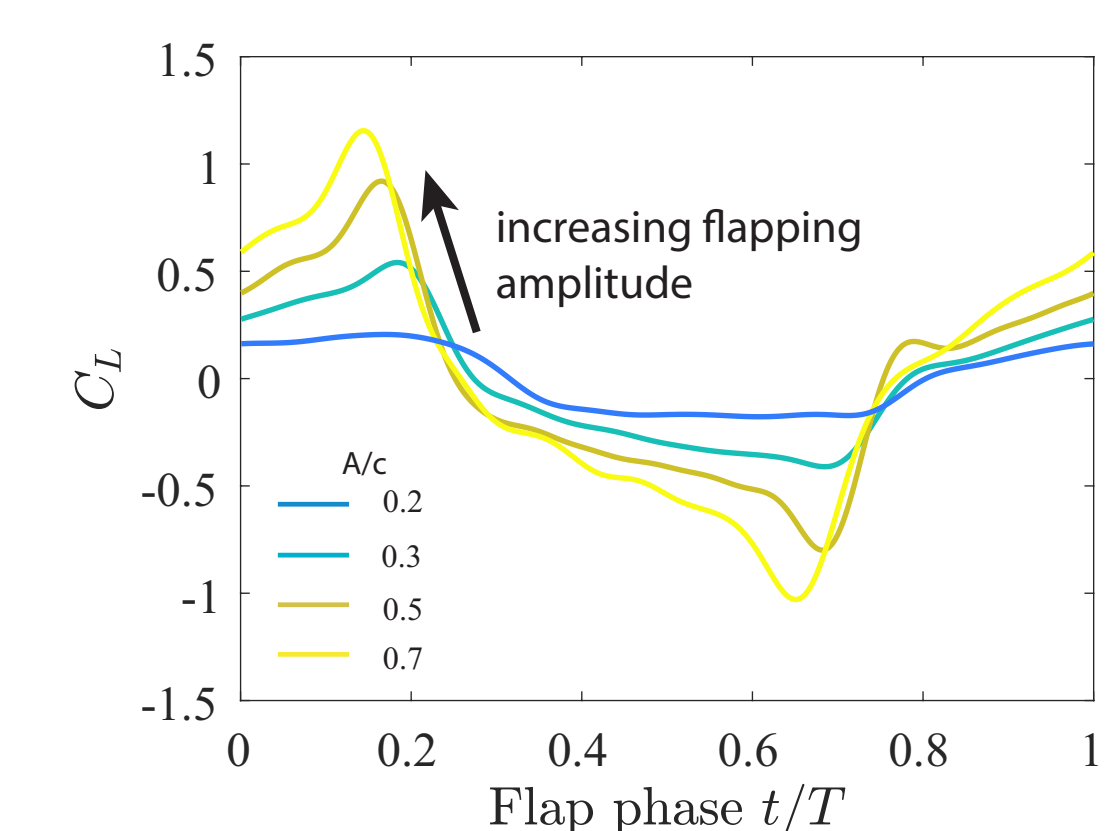
CONCLUSIONS

- The force response of the surfing wing is aligned with the impingement of flow structures
- The wing's lift response frequency locks to the wake-generating frequency, with cycle-level fluctuations scaling with Strouhal number.
- A predictive model leveraging classic unsteady aerodynamics to account for structured wake interactions, with theoretical predictions closely aligning with force sensor data—particularly when using the Wagner approach in the time domain.

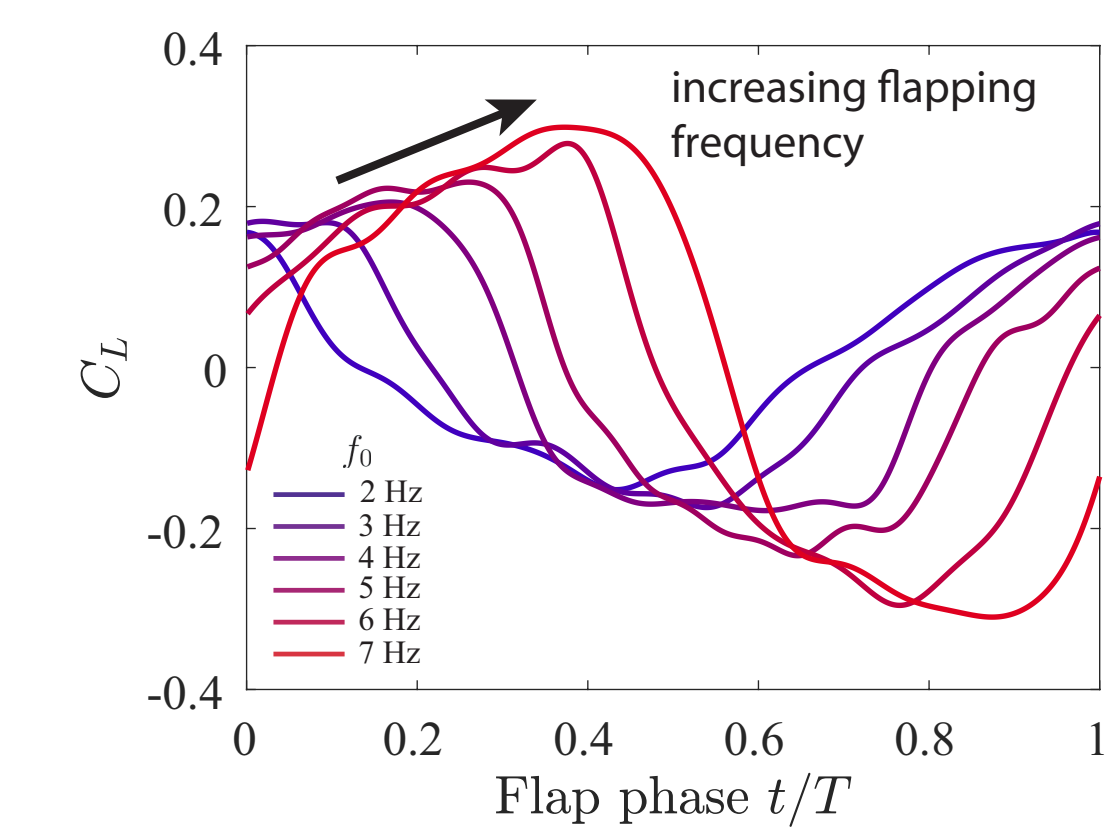
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- a.** In low St case, **down wash** and **up wash** are induced from strokes
- b.** In high St case, a primary **CCW** vortex shed in the first half-stroke, as it approaching, the surfing airfoil sees an increment in lift coefficient. The lift coefficient reach the peak on the impingement ($t/T = 0.18$) with a separation bubble initiated on LE. As the separation growing, the lift coefficient falls back to neutral ($t/T = 0.25$). The **symmetric** process repeat in the other half-stroke.



c. Lift vs. flapping amplitude at fixed flapping frequency



d. Lift vs. flapping frequency at fixed flapping amplitude